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# Adsorptive removal of arsenic from water by an iron-zirconium binary oxide adsorbent

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#### ABSTRACT

Arsenate and arsenite may exist simultaneously in groundwater and have led to a greater risk to human health. In this study, an iron–zirconium (Fe–Zr) binary oxide adsorbent for both arsenate and arsenite removal was prepared by a coprecipitation method. The adsorbent was amorphous with a specific surface area of 339 m<sup>2</sup>/g. It was effective for both As(V) and As(III) removal; the maximum adsorption capacities were 46.1 and 120.0 mg/g at pH 7.0, respectively, much higher than for many reported adsorbents. Both As(V) and As(III) adsorption occurred rapidly and achieved equilibrium within 25 h, which were well fitted by the pseudo-second-order equation. Competitive anions hindered the sorption according to the sequence  $PO_4^{3-} > SO_3^{2-} > SO_4^{2-}$ . The ionic strength effect experiment, measurement of zeta potential, and FTIR study indicate that As(V) forms inner-sphere surface complexes, while As(III) forms both inner- and outer-sphere surface complexes at the water/Fe–Zr binary oxide interface. The high uptake capability and good stability of the Fe–Zr binary oxide make it a potentially attractive adsorbent for the removal of both As(III) from water.

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#### 1. Introduction

Arsenic is ubiquitous in the environment and of worldwide serious concern due to its high toxicity and carcinogenicity. Long-term drinking water exposure causes cancer of the liver, lung, kidney, bladder, and skin as well as skin thickening (hyperkeratosis), neurological disorders, muscular weakness, and loss of appetite and nausea [1–3]. To minimize these health risks, a strict guideline limit of 10 ppb (10  $\mu$ g/L) provided by the World Health Organization (WHO) [4] has been adopted as the drinking water standard by many countries.

In natural waters, arsenic occurs predominantly in inorganic form as arsenate and arsenite, referred to as As(V) and As(III). As(III) is much more toxic [5], soluble, and mobile than As(V). A variety of treatment processes such as coagulation/precipitation [6,7], ion-exchange [8], adsorption [4,9,10], and membrane processes [8,11] have been employed to remove arsenic. Adsorption methods are considered to be the most promising technologies because the system can be simple to operate and cost-effective [10]. However, most adsorbents, both natural and synthetic materials, are effective for As(V) [12,13], but fail in the case of As(III) [14,15]. To achieve higher arsenic removal, pretreatment for As(III) oxidation is therefore usually involved, followed by sorption of the As(V) formed onto metal oxyhydroxides. But the pretreatment results not only in higher run cost but also in more complex operation. Therefore, there is urgent demand for economical, effective, and reliable adsorbents that are capable of removing both As(V) and As(III) simultaneously from contaminated drinking water.

Among a variety of available sorbents for arsenic removal, iron (hydr)oxides, including amorphous hydrous ferric oxide, poorly crystalline hydrous ferric oxide (ferrihydrite), goethite, and akaganéite [12,16,17], are well-known for their high affinity toward arsenic, low cost, and environmental friendliness. Recently, the development of composite adsorbents containing iron oxide has gained considerable attention [18–20], since they have advantages over these components. For examples, an Fe–Ce bimetal oxide adsorbent synthesized by Zhang et al. [18] exhibited a much higher As(V) adsorption capacity than individual Ce and Fe oxides is prepared by the same procedure. A novel Fe–Mn binary oxide adsorbent developed by Zhang et al. [19] demonstrated enhanced arsenite removal through oxidization and then adsorption. Gupta and Ghosh [20] reported the synthesis and use of Fe–Ti binary mixed oxide for arsenic sorption.

Hydrous zirconium oxide, with high resistance to attacks by acids, alkalis, oxidants, and reductants, is more suitable for the adsorption of arsenite than iron oxide [21]. Therefore, it can be anticipated that an Fe–Zr binary oxide would simultaneously be able to remove both arsenate and arsenite effectively.

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However, few studies are available in the literature on arsenic removal by Fe–Zr binary oxides. Gupta et al. demonstrated that a nanostructure iron(III)–zirconium(IV) binary mixed oxide with an Fe/Zr molar ratio of 9:1 was much more effective for arsenite than arsenate removal [22,23]. However, the maximum adsorption capacity for arsenate was only 9.36 mg/g. In addition, the synthetic route involved a process of heating, which was not favorable for large-scale production of sorbent. It is therefore necessary to develop new synthetic routes by which Fe–Zr binary oxide could be synthesized under milder conditions and be effective for both arsenate and arsenite removal.

In this study, a simple coprecipitation method was established to prepare an innovative Fe–Zr binary oxide adsorbent at ambient temperature. The main objectives of this research were (1) to characterize the prepared Fe–Zr binary oxide by a variety of techniques; (2) to evaluate its arsenic adsorption capacities and examine the influence of solution pH, ionic strength, and coexisting ions on arsenic adsorption; and finally; (3) to explain the adsorption mechanisms for both arsenate and arsenite.

#### 2. Materials and methods

#### 2.1. Materials

All chemicals are analytical grade and used without further purification. Reaction vessels (glass) were cleaned with 1% HNO<sub>3</sub> and rinsed several times with deionized water before use. As(III) and As(V) stock solutions were prepared with deionized water using NaAsO<sub>2</sub> and NaHAsO<sub>4</sub>·7H<sub>2</sub>O, respectively. Arsenic working solutions were freshly prepared by diluting arsenic solutions with deionized water.

#### 2.2. Preparation of Fe-Zr binary oxide

The Fe–Zr binary oxide was prepared according to the following procedure: Ferric chloride hexahydrate (FeCl<sub>3</sub>·6H<sub>2</sub>O, 0.05 mol) and zirconyl chloride octahydrate (ZrOCl<sub>2</sub>·8H<sub>2</sub>O, 0.0125 mol) were dissolved in 400 ml deionized water. Under vigorous magnetic stirring, sodium hydroxide solution (2 mol/L) was added dropwise to raise the solution pH to around 7.5. After addition, the suspension formed was continuously stirred for 1 h, aged at room temperature for 4 h, and then washed several times with deionized water. The suspension was then filtrated and dried at 65 °C for 4 h. The dry material was crushed and stored in a desiccator for use. The obtained material appeared in the form of a fine powder.

#### 2.3. Adsorbent characterization

X-ray diffraction (XRD) analysis was carried out on a D/Max-3A diffractometer (Rigaku Co., Japan) using Ni-filtered copper K $\alpha_1$  radiation. The specific surface area was measured by nitrogen adsorption using the BET method with a Micromeritics ASAP 2000 surface area analyzer (Micromeritics Co., USA). The particle size of the adsorbent was determined by a Mastersizer 2000 (Malvern Co., UK). The particle shapes were observed using a Hitachi S-3500N (Hitachi Co., Japan) scanning electron microscope (SEM).

A zeta potential analyzer (Zetasizer 2000, Malvern Co., UK) was used to analyze the zeta potentials of Fe–Zr binary oxide particles before and after arsenic adsorption. The content of the Fe–Zr binary oxide in the solution was about 200 mg/L and the initial arsenic concentration was 10 mg/L. NaNO<sub>3</sub> was used as a background electrolyte to maintain an approximately constant ionic strength of 0.01 M. After being mixed for 72 h to ensure the achievement of adsorption equilibrium, 20 ml of oxide suspension was transferred to a sample tube. The zeta potential of the suspension was then measured by electrokinetic analysis.

FTIR spectra were collected on a Nicolet 5700 FTIR spectrophotometer (Nicolet Co., USA) using a transmission model. Samples for FTIR determination were ground with spectral grade KBr in an agate mortar. IR spectra of arsenate adsorbed onto Fe–Zr binary oxide were obtained as dry samples in KBr pellets corresponding to 5 mg of sample in approximately 200 mg of spectral grade KBr. All IR measurements were carried out at room temperature.

X-ray photoelectron spectra (XPS) were collected on an ESCA-Lab-220i-XL spectrometer with a monochromatic Al K $\alpha$  X-ray source (1486.6 eV). C1s peaks were used as an inner standard calibration peak at 284.7 eV. For wide-scan spectra, an energy range of 0–1100 eV was used with pass energy 80 eV and step size 1 eV. The high-resolution scans were conducted according to the peak being examined with pass energy 40 eV and step size 0.05 eV. The XPS results were collected in binding energy forms and fitted using a nonlinear least-squares curve-fitting program (XPSPEAK41 Software).

#### 2.4. Batch adsorption tests

#### 2.4.1. Adsorption kinetics

The rate of arsenic adsorption is an important factor in arsenic removal. The kinetics experiments were carried out at room temperature ( $25 \pm 1 \circ C$ ). A defined amount of arsenic stock solution was added in a 1000-ml glass vessel. Then, a corresponding amount of deionized water was added to make 750 ml of 5, 10, 20 mg/L arsenic solution. The ionic strength was maintained at 0.01 M by adding 0.638 g sodium nitrate. After the solution pH was adjusted to 7.0 ± 0.1 by adding 0.1 M HCl and/or NaOH, 0.15 g of Fe-Zr binary oxide was added to obtain a 0.2 g/L suspension. The suspension was mixed with a magnetic stirrer at an agitation speed of 140 rpm, and the pH was maintained at  $7.0 \pm 0.1$ throughout the experiment by addition of dilute acid and/or base solutions. Approximately 5-ml aliquots were taken from the vessel at predetermined times. The samples were immediately filtered through a 0.45-um membrane filter. The concentrations of arsenic in the filtered solutions were determined using inductively coupled plasma atomic emission spectroscopy (ICP-AES).

#### 2.4.2. Effect of pH and ionic strength

To investigate the influence of pH and ionic strength on the arsenic adsorption, experiments were carried out by adding 10 mg of the adsorbent sample into 150-ml glass vessels, containing 50 ml of 10 mg/L arsenic solution. The ionic strength of the solutions was varied from 0.001 M to 0.1 M by adding NaNO<sub>3</sub>.The pH of the solutions was adjusted every 4 h with dilute HNO<sub>3</sub> or/and NaOH solution to designated values in the range 3–12 during the shaking process. The equilibrium pH was measured and the supernatant was filtered through a 0.45-µm membrane after the solutions were mixed for 36 h. Then the residual arsenic concentration in the supernatant solutions was determined. Additionally, to evaluate the leaching of Fe and Zr from the adsorbent at different pHs, the Fe and Zr concentrations in the supernatant solutions were also measured using ICP–AES.

#### 2.4.3. Adsorption isotherms

The arsenic adsorption isotherm was determined using batch tests at the initial pH values of  $7.0 \pm 0.1$ . Initial arsenic concentration was varied from 5 to 40 mg/L. In each test, 10 mg of the adsorbent sample was loaded in the 150-ml glass vessel and 50 ml of solution containing different amounts of arsenic was then added to the vessel. Ionic strength of the solution was adjusted to 0.01 M with NaNO<sub>3</sub>. The vessels were shaken on an orbit shaker at 140 rpm for 36 h at  $25 \pm 1$  °C. After the reaction period, all

samples were filtered by a 0.45-µm membrane filter and analyzed for arsenic. The quantity of adsorbed arsenic was calculated by the difference of the initial and residual amounts of arsenic in solution divided by the weight of the adsorbent.

#### 2.4.4. Effect of coexisting ions

The influence of common coexisting anions in water such as sulfate, bicarbonate, silicate, and phosphate on the removal of arsenic was investigated by adding sodium sulfate, sodium bicarbonate, sodium silicate, and sodium phosphate to 10 mg/L of arsenic solution. In addition, the effect of calcium and magnesium ions on arsenic adsorption was also studied by adding lime nitrate and magnesium nitrate into arsenic solution. The solution pH was adjusted to  $7.0 \pm 0.1$ . A defined amount (10 mg) of Fe–Zr binary oxide was added and the solutions were agitated at 140 rpm for 36 h at  $25 \pm 1$  °C. After filtration by a 0.45-µm membrane filter, the residual concentration of arsenic was analyzed using ICP–AES.

#### 2.5. Analytical methods

Arsenic concentration was determined using ICP–AES (Optima 2100 DV, Perkin Elmer Co., USA). Prior to analysis, the aqueous samples were acidified with concentrated HCl in an amount of 1% and stored in acid-washed glass vessels. All samples were analyzed within 24 h of collection.

#### 3. Results and discussion

#### 3.1. Characterization of prepared Fe-Zr binary oxide

The powder X-ray diffraction pattern of the synthesized Fe–Zr binary oxide is illustrated in Fig. 1. It shows two broad peaks at approximately  $35.2^{\circ}$  and  $61.2^{\circ}$ , consistent with d spacing of 0.254 and 0.150 nm, respectively, which are similar to those of the poorly ordered two-line ferrihydrite [24,25]. This indicates that the prepared oxide is amorphous and similar to two-line ferrihydrite.

The morphology of the Fe–Zr binary oxide was examined by a scanning electron microscope. Fig. 2 shows that the adsorbent particles are aggregated with many nanoparticles, leading to a rough surface and a porous structure. The distribution of particle size of the powdered adsorbent is shown in Fig. S1 (Supplementary materials), indicating that the main particle size of this binary oxide is in the range 2–30  $\mu$ m. BET analysis shows that the sorbent has a specific surface area of 339 m<sup>2</sup>/g with a pore volume of 0.21 cm<sup>3</sup>/g. The pore size distribution of this sorbent is shown in Fig. S2. The sorbent presented a wide pore size range from 50 to below 1.5 nm.

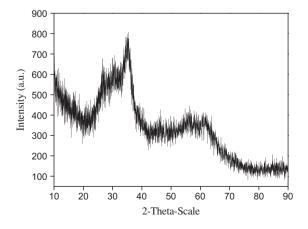


Fig. 1. XRD diffraction pattern of Fe–Zr binary oxide with a Fe/Zr molar ratio of 4:1.

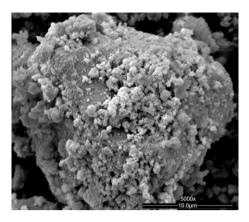


Fig. 2. SEM micrograph (×5000) of Fe–Zr binary oxide particles.

The concentrations of dissolved Fe and Zr under different pH are shown in Fig. S3. The Fe concentrations are all below 0. 06 mg/L<sup>1</sup> and the Zr concentrations all below 0.01 mg/L<sup>1</sup> in the tested pH range, which are far below the limit of drinking water standard [26]. Very limited metal leakage would not cause metal contamination in the environment, indicating the good stability of this adsorbent.

#### 3.2. Adsorption kinetics

The adsorption kinetics of arsenic on Fe–Zr binary oxide at various initial concentrations was investigated in this study. Fig. 3 shows the change of adsorbed arsenic as a function of contact time. It is obvious that the adsorption process can be divided into two steps. In the first rapid step, over 80% of the equilibrium adsorption capacity is achieved within 4 h. In the following step, intraparticle diffusion dominates and the adsorption slows down. The time taken to reach equilibrium is about 25 h. Therefore, for all other batch experiments, the contact time was maintained as 36 h, higher than the equilibrium time of 25 h, to ensure complete adsorption. Adsorption due solely to electrostatic processes is usually very rapid, on the order of seconds [17]. The adsorption of arsenic by the Fe–Zr binary oxide is on the order of hours, which may indicate specific adsorption occurring between the arsenic species and the surface of the adsorbent.

Kinetic data analysis for arsenic sorption onto the Fe–Zr binary oxide was studied with a pseudo-first-order model [27] and a pseudo-second-order model [28]. The mathematical representations of the models are given in

$$\ln(q_e - q_t) = \ln q_e - k_1 t \tag{1}$$

$$\frac{t}{q_t} = \frac{1}{k_2 q_e^2} + \frac{t}{q_e} \tag{2}$$

where  $q_e$  and  $q_t$  are the adsorption capacities (mg/g) of the adsorbent at equilibrium and at any time *t* (h), respectively; and  $k_1$  (h<sup>-1</sup>) and  $k_2$  (g mg/h) are the related adsorption rate constants.

The rate constants obtained from pseudo-first-order and pseudo-second-order models are summarized in Table 1. For both arsenate and arsenite, the experimental data fitted the pseudo-second-order model better than the pseudo-first-order model. This indicates that the adsorption process might be chemisorption. The rate constant of the pseudo-second-order equation decreases with increasing initial arsenic concentration, indicating that arsenic adsorption may be more favorable at low solute concentration. Furthermore, the values of  $k_2$  for As(III) adsorption are higher than those for As(V) adsorption. This suggests that the removal of As(III) is faster than that of As(V). Similar results are observed for adsorption of As(V) and As(III) by ferrihydrite [29]

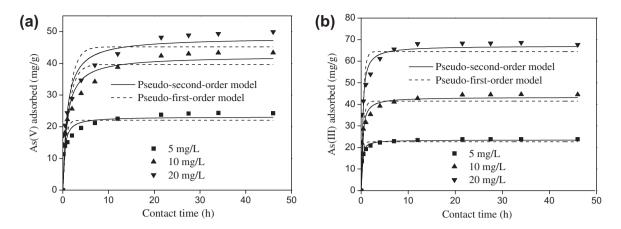


Fig. 3. Kinetics of (a) As(V) and (b) As(III) removal by Fe–Zr binary oxide at different initial concentrations: (■) 5 mg/L, (▲) 10 mg/L, (▼) 20 mg/L. Adsorbent dose = 200 mg/L, pH = 7.0 ± 0.1, agitation speed = 130 rpm, T = 25 ± 1 °C.

## Table 1 Adsorption rate constant obtained from pseudo-first-order model and pseudo-second-order model for various initial concentrations of arsenic.

Arsenic species	Initial concentration (mg/L)	Pseudo-first-order model			Pseudo-second-order model		
		$\frac{k_1}{(h^{-1})}$	q <sub>e</sub> (mg/g)	<i>R</i> <sup>2</sup>	k <sub>2</sub> (g/mg h)	q <sub>e</sub> (mg/g)	<i>R</i> <sup>2</sup>
As(V)	5	1.892	22.1	0.838	0.129	23.1	0.933
	10	0.758	39.7	0.858	0.027	42.3	0.938
	20	0.720	45.2	0.845	0.023	48.3	0.927
As(III)	5	3.958	22.6	0.933	0.294	23.8	0.987
	10	2.614	41.5	0.895	0.096	43.3	0.969
	20	2.402	64.5	0.886	0.060	67.1	0.963

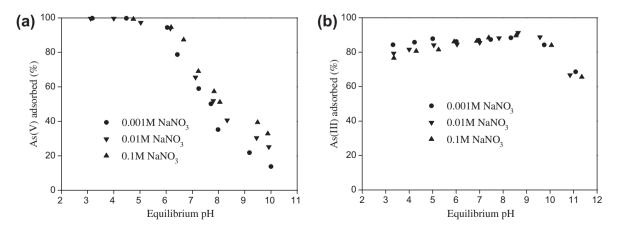
or nanocrystalline titanium dioxide [30]. The kinetics experiments presented in Fig. 4 were carried out at pH 7.0  $\pm$  0.1. At this pH, the surface potential of Fe–Zr binary oxide is negative (see Section 3.7). As(V) is largely present as negatively charged H<sub>2</sub>AsO<sub>4</sub><sup>-</sup> and HAsO<sub>4</sub><sup>2-</sup> species, while As(III) is present at neutral H<sub>3</sub>AsO<sub>3</sub> species. The higher adsorption rate of As(III) than of As(V) could be attributed to the lower electrostatic repulsion between the surface and the As(III) species.

A multiexponential equation was also used to fit the kinetic data, and the results and detailed discussion are shown in the Supplementary materials.

#### 3.3. Effect of pH and ionic strength

The effects of pH and ionic strength on the removal of As(V) and As(III) were studied. As can be seen from Fig. 4a, As(V) adsorption is evidently dependent on pH, with the greatest adsorption occurring under acidic conditions, and decreases with an increase in solution pH. Adsorption of strong acid anions by metal oxides and hydroxides typically decreases with increasing pH [31]. Such a pH effect was observed for the sorption of As(V) onto iron oxides or iron-containing oxides [32,33].  $H_2AsO_4^-$  and  $HAsO_4^{2-}$  are dominant As(V) species in the solution in the tested pH range (3-10). Lower pH is favorable for the protonation of the sorbent surface. Increased protonation is thought to increase the positively charged sites, enlarge the attraction force existing between the sorbent surface and arsenate anions, and therefore increase the amount of adsorption in the lower pH region. With the increase in solution pH, the negatively charged sites gradually dominate, the repulsion effect is enhanced, and the amount of adsorption consequently falls.

In contrast, As(III) adsorption gradually increases with increasing solution pH and reaches a maximum at pH approximately 9.0 (Fig. 4b). Adsorption of weak acids by metal oxides usually reaches a maximum at pH values similar to the  $pk_{a1}$  of the acid [31]. The  $pk_{a1}$  of arsenious acid is 9.2. The decrease in As(III) sorption at pH over 9.0 may be due to the coulombic repulsion between As(III)



**Fig. 4.** Effect of pH and ionic strength on As(V) (a) and As(III) (b) adsorption on Fe–Zr binary oxide. Initial arsenic concentration = 10 mg/L; adsorbent dose = 200 mg/L; agitation speed = 140 rpm,  $T = 25 \pm 1$  °C.

species and the negative surfaces of the Fe–Zr binary oxide  $(pH_{ipe} = 5.1)$ .

Anions that are adsorbed through outer-sphere association are strongly sensitive to ionic strength; the adsorption is suppressed by competition with weakly adsorbing anions such as  $NO_3^-$ , since electrolytes also form outer-sphere complexes through electrostatic forces. Conversely, anions that are adsorbed by the innersphere association either show little sensitivity to ionic strength or respond to higher ionic strength with greater adsorption [34]. For As(V), the increase in ionic strength from 0.001 to 0.1 M leads to a shift in the position of the pH edge toward the alkaline region (Fig. 4a), and slightly enhances adsorption in this range (7–10). These behaviors are indicative of an inner-sphere adsorption mechanism for As(V) on the Fe–Zr binary oxide. A similar phenomenon was observed by Deliyanni and co-workers [35] when they studied the adsorption of As(V) on akaganéite.

For As(III), the change in ionic strength does not significantly influence its sorption on the Fe–Zr binary oxide above pH 6. This suggests an inner-sphere adsorption mechanism involved in the sorption. However, As(III) adsorption below pH 6 decreased with increasing ionic strength, suggesting an outer-sphere adsorption mechanism.

#### 3.4. Adsorption isotherms

Adsorption isotherms for both As(III) and As(V) were obtained at  $7.0 \pm 0.1$  by varying the initial arsenic concentrations (5– 50 mg/L). The isotherms thus obtained are presented in Fig. 5. Obviously, the adsorbent has a much higher adsorption capacity for As(III) than that of As(V). Both Langmuir and Freundlich models [36,37] were employed to describe the adsorption isotherms obtained in the figure. The Freundlich equation is represented as

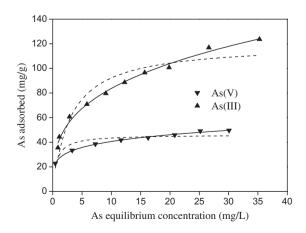
$$q_e = K_F C_e^n, \tag{3}$$

where  $q_e$  is the amount of arsenic adsorbed onto the solid phase (mg/g),  $C_e$  is the equilibrium arsenic concentration in the solution phase (mg/L),  $K_F$  is roughly an indicator of the adsorption capacity, and n is the heterogeneity factor, which has a lower value for more heterogeneous surfaces.

The Langmuir equation can be written in the form

$$q_e = \frac{q_{\max} bC_e}{1 + bC_e},\tag{4}$$

where  $q_e$  and  $C_e$  are as previously denoted, *b* is the equilibrium adsorption constant related to the affinity of binding sites (L/mg),



**Fig. 5.** Isotherms for As(III) and As(V) adsorption by Fe–Zr binary oxide at pH 7.0  $\pm$  0.1 and  $T = 25 \pm 1$  °C; (–) Langmuir model and (–) Freundlich model.

and  $q_{max}$  is the maximum amount of the arsenic per unit weight of adsorbent for complete monolayer coverage.

The adsorption constants obtained from the isotherms are listed in Table 2. It is seen that the Freundlich model fits the experimental data reasonably well. The Langmuir model is, however, unsuitable for describing the adsorption of arsenic by Fe-Zr binary oxide, due to a relatively poor correlation coefficient ( $R^2 < 0.90$ ). The Langmuir isotherm fails to describe the adsorption behavior because it assumes that adsorption occurs on a homogeneous surface. The presence of zirconium dioxide in the adsorbent may lead to a more heterogeneous surface. The Freundlich equation describes adsorption where the adsorbent has a heterogeneous surface with adsorption sites that have different energies of adsorption. The calculated Langmuir adsorption capacities for As(V) and As(III) are 46.1 and 120.0 mg/g, respectively. This suggested that Fe–Zr adsorbent is effective for both As(V) and As(III) removal, particularly the latter. To assess the arsenic removal performance of Fe-Zr binary oxide, the  $q_{\text{max}}$  values are compared with the reported values (Table 3). It is found that the prepared Fe-Zr binary oxide outperforms many other adsorbents. Especially, the values of maximal adsorption capacities of As(V) and As(III) obtained in the present study are nearly four times and one time higher than the nano-Fe(III)-Zr(IV) mixed oxide [22,23].

#### 3.5. Effect of coexisting anions

Anions such as sulfate, bicarbonate, silicate, and phosphate are generally present in water, and could interfere in the uptake of arsenic through competitive adsorption. Thus, the influences of these anions at three concentration levels (0.1, 1.0, and 10 mM) on the arsenic removal were assessed at pH 7.0  $\pm$  0.1. The experimental results are presented in Fig. 6.

It is clear that the coexisting sulfate had no significant influence on the As(V) removal. Only a 5% reduction in As(V) removal rate is observed even when the sulfate concentration is as high as 10 mM.

#### Table 2

Table 3

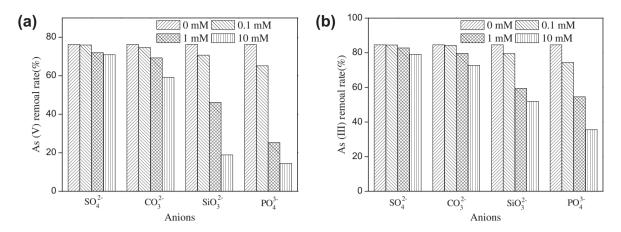
Langmuir and Freundlich isotherm parameters for As(V) and As(III) adsorption onto Fe–Zr binary oxide at pH 7.0  $\pm$  0.1.

As species	Langmuir model			Freundlich model		
	$q_m (\mathrm{mg/g})$	$K_L$ (L/mg)	$R^2$	$K_F(mg/g)$	n	$R^2$
As(V) As(III)	46.1 120.0	1.611 0.332	0.788 0.894	26.6 40.8	0.183 0.311	0.996 0.992

Tuble 5					
Comparison of	f maximum arseni	c adsorption	capacities f	or different	adsorbents <sup>a</sup>

•				
Adsorbent	Conc. range (mg/L)	Max. As(III) adsorption capacity (mg/g)	Max. As(V) adsorption capacity (mg/g)	Ref.
Fe-Zr binary oxide	5-40	120.0 (pH 7.0)	46.1 (pH 7.0)	Present study
Fe-Mn binary oxide	5-40	132.7 (pH 5.0)	69.8 (pH 5.0)	[19]
Nano-Fe(III)-Ti(IV) mixed oxide	5.0- 250	85.0 (pH 7.0)	14.3 (pH 7.0)	[20]
Nano-Fe(III)–Zr(IV) mixed oxide	5-350	64.5–66.5 (pH 7.0)	9.36 (pH 7.0)	[22,23]
Akaganeite nanocrystals	5-25	-	134.1 (pH 7.5)	[35]
Nano-TiO <sub>2</sub>		59.9 (pH 7.0)	37.5 (pH 7.0)	[30]
$Al_2O_3/Fe(OH)_3$	7.5– 135	9.0 (pH 6.6)	36.7 (pH 7.2)	[38]
CuO nanoparticle	0.1– 100	26.9 (pH 8.0)	22.6 (pH 8.0)	[39]
Zr-based magnetic sorbent	0-100	-	45.6 (pH 5.0- 6.0)	[40]

<sup>a</sup> pH is shown in parentheses.



**Fig. 6.** Effects of co-existing anions on (a) As(V) and (b) As(III) removal at fixed initial arsenic concentration = 10 mg/L. Adsorbent dose = 200 mg/L, pH = 7.0  $\pm$  0.1, agitation speed = 140 rpm,  $T = 25 \pm 1$  °C.

The presence of bicarbonate slightly decreases the removal of As(V). However, the coexisting silicate and phosphate greatly hindered the As(V) adsorption.

The As(III) removal is less affected by these anions than that of As(V), as shown in Fig. 6b. Among the anions, phosphate causes the greatest decrease in arsenic adsorption, which may be due to the strong competition for the binding sites of the adsorbent between the phosphate and arsenic. Both phosphate and arsenic are located in the same main group, and the molecular structure of the phosphate ion is very similar to that of the arsenic ion. Thus, the present phosphate ions must strongly compete with arsenic ions for adsorptive sites on the surfaces of Fe–Zr binary oxides.

#### 3.6. Zeta potential measurement

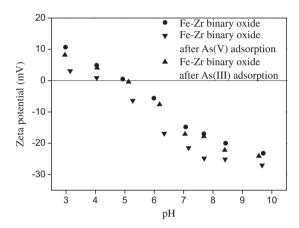
The zeta potentials of the Fe–Zr binary oxide suspensions before and after arsenic adsorption were measured. As shown in Fig. 7, the Fe–Zr binary oxide has an isoelectric point of about 5.1, which was decreased to about 4.1 after As(V) adsorption. However, the isoelectric point is not significantly changed after the As(III) adsorption. The specific adsorption of anions makes the surface of oxides more negatively charged, which results in a shift of the isoelectric point of adsorbent to a lower pH value [41,42].

For As(V), specific adsorption rather than purely electrostatic interaction is further confirmed from the drop of isoelectric point at the aqueous arsenate/Fe–Zr binary oxide interface. However, lack of shift in IEP cannot be used to infer an outer-sphere adsorption mechanism, since inner-sphere surface complex formation is not necessarily accompanied by a change in the mineral surface [43]. For As(III), no obvious change in the isoelectric point of the Fe–Zr binary oxide is observed after its sorption, which indicates the formation of either an outer-sphere surface complex or an inner-sphere complex that may not change the surface charge.

#### 3.7. Analysis of XPS and FTIR spectra

XPS spectra of Fe–Zr binary oxide and samples after arsenic adsorption were collected to verify the presence of arsenic and determine the oxidation state of adsorbed arsenic. Fig. 8 shows the presence of the As3d core level peak as well as the AsLMM and As3p peaks, which clearly indicates the adsorption of As(V) and As(III) onto the sorbent.

Fig. 9 exhibits the As3d core level of the Fe–Zr binary oxide after the adsorption of As(V) and As(III). The As3d binding energies are 45.5 and 44.4 eV, respectively. The values of the binding energy



**Fig. 7.** Zeta potential of Fe–Zr binary oxide before and after arsenic adsorption at initial arsenic concentration = 10 mg/L. Adsorbent dose = 200 mg/L, ionic strength = 0.01 M NaNO<sub>3</sub>, equilibrium time = 72 h.

of the As3d core level for As(III) and As(V) in arsenic oxides are reportedly 44.3–44.5 and 45.2–45.6 eV, respectively [44,45]. They can be shifted up to 44.6  $\pm$  0.13 eV for As(III) and 46.0  $\pm$  0.17 eV for As(V) when the arsenic anions or molecules are adsorbed onto iron oxide [46]. It can therefore be concluded that the arsenic species adsorbed onto the surface of the Fe–Zr oxide after the binding of As(V) and As(III) still remain as As(V) and As(III), respectively. In other words, the oxidation state of As(III) is not changed during the adsorption process.

More useful information about the interaction between aqueous arsenic and solid Fe-Zr binary oxide can be provided by the FTIR technique. Fig. 10 shows the FTIR spectra in which spectrum (a) is for original Fe–Zr binary oxide, spectrum (b) for Fe–Zr binary oxide treated with 40 mg/L As(III) solution at pH 7.0, and spectrum (c) for Fe-Zr binary oxide treated with of Fe-Zr binary oxide mg/L As(V) solution at pH 7.0. For the Fe–Zr binary oxide sample, the bands at 3400 cm<sup>-1</sup> may be assigned to the vibration of O-H stretching and 1630 cm<sup>-1</sup> may be assigned to the deformation vibration of water molecules, indicating the presence of physisorbed water on the oxide. For the As(V)-treated sample, a new peak at 827 cm<sup>-1</sup> could be assigned to the vibration (As–OH) of As–O–Fe groups [43]. This indicates that the As(V) is mainly bound as a surface complex. However, no obvious change can be observed in the spectrum of the As(III)-loaded adsorbent. In fact, in contrast to the spectra of As(V) sorbed into Fe oxides, it is difficult to detect the presence of sorbed As(III) on the surface of Fe oxides [43].

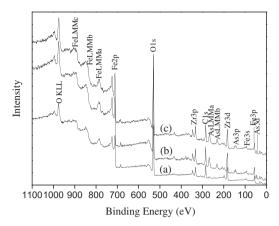


Fig. 8. XPS spectra of Fe–Zr binary oxide (a) as prepared; (b) after reaction with As(V); and (c) after reaction with As(III).

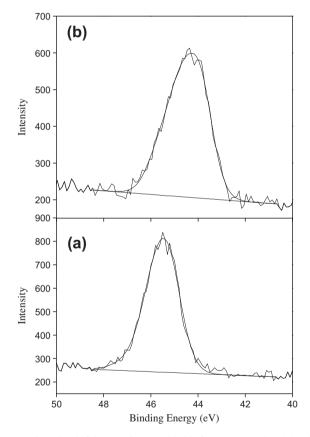
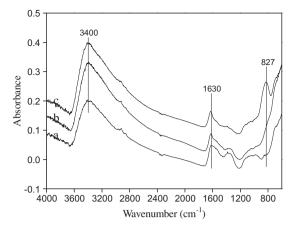


Fig. 9. As3d core level of the Fe–Zr binary oxide (a) after reaction with As(V) and (b) after reaction with As(III).

From the results of the ionic strength effects experiment and the analyses of zeta potential along with FTIR spectra, reasonable mechanisms for arsenic adsorption on the Fe–Zr binary oxide can be provided. As(V) is adsorbed by formation of inner-sphere surface complexes, while As(III) is adsorbed by formation of both inner- and outer-sphere surface complexes. Fig. 11 demonstrates the proposed mechanisms.

#### 4. Conclusions

The preparation of Fe–Zr binary oxide is a simple and environmentally friendly method. This adsorbent, with a high surface area



**Fig. 10.** FTIR spectra of Fe–Zr binary oxide (a), after treatment with As(III) solution of 40 mg/L (b), and after treatment with As(V) solution of 40 mg/L (c).

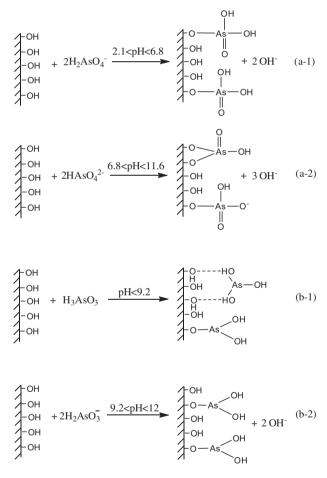


Fig. 11. Schematic diagram of adsorption mechanisms of As(V) (a) and As(III) (b).

 $(339 \text{ m}^2/\text{g})$ , was amorphous. The pseudo-second-order equation describes the kinetic data well. The adsorbent had a high removal capacity toward both As(V) and As(III). Maximal adsorption capacities were 46.1 mg/g and 120.0 mg/g at pH 7.0, respectively. The Fe–Zr binary oxide is able to adsorb arsenic in the presence of competing anions and across a wide range of pH. Among the coexisting anions, phosphate was the greatest competitor with arsenic for adsorptive sites on the surface of oxide. The results of ionic strength effects experiment and analyses of zeta potential and FTIR

spectra indicate that As(V) forms inner-sphere surface complexes, while As(III) forms both inner- and outer-sphere surface complexes at the water/Fe–Zr binary oxide interface.

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#### Appendix A. Supplementary material

Supplementary data associated with this article can be found, in the online version, at doi:10.1016/j.jcis.2011.01.013.

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